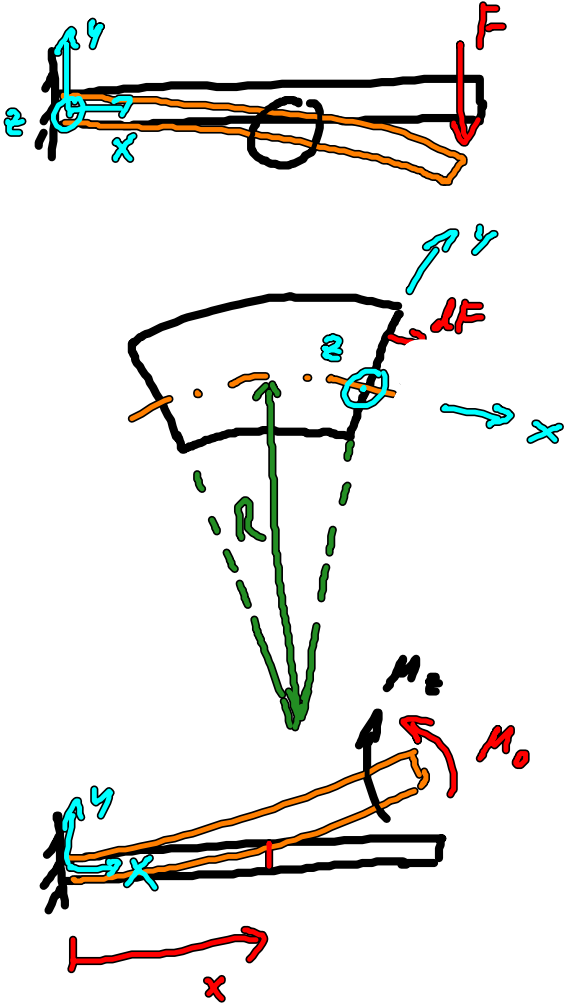


VL-22 : Spannungsverteilung bei Biegung

I) Spannungsverteilung :

VL-17:

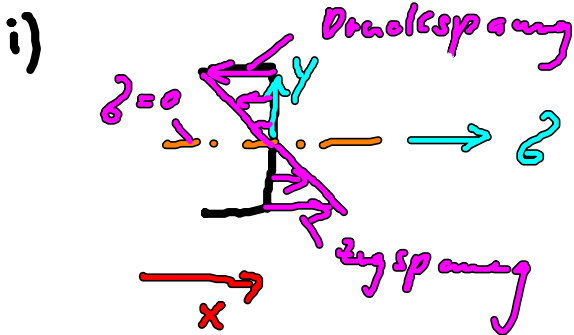


$$\sigma = E \epsilon = E \frac{y}{R}$$

$$M_F = - \int y dF = - \frac{E I_z}{R}$$

$$\Rightarrow \sigma = - \frac{M_z}{I_z} \cdot y$$

$$M_z = M_0 \Rightarrow \sigma = - \frac{M_0}{I_z} \cdot y$$



maximale Spannung:

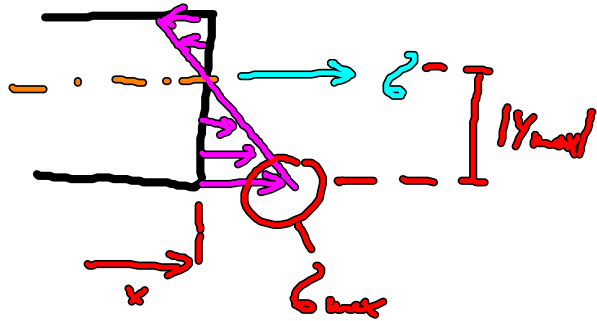
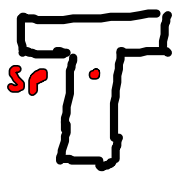
$$\left[\sigma_{max} = \left| \frac{M_{max}}{I_z} y_{max} \right| = \frac{|M_{max}|}{W} \right]$$

$$\frac{I_z}{|y_{max}|} = W$$

Widerstandsmoment

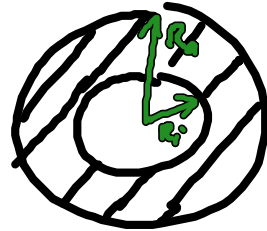
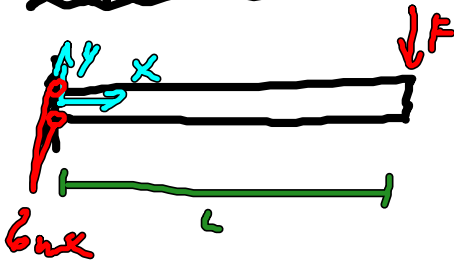
ii)





innere Spannung
an allen Rand

Beispiel 1



$$R_a = 5 \text{ cm}$$

$$R_i = 4 \text{ cm}$$

$$L = 3 \text{ m}$$

ges: F damit $\sigma \leq \sigma_{zul} = 150 \text{ MPa}$

$$\left\{ \sigma = \frac{M}{I} y, \quad \sigma_{max} = \frac{|M_{max}|}{W}, \quad W = \frac{I_0}{|y_{max}|} \right\}$$

$$\frac{|M_{max}|}{W} \leq \sigma_{zul}, \quad \text{mit: } |M_{max}| = F \cdot L, \quad |y_{max}| = R_a$$

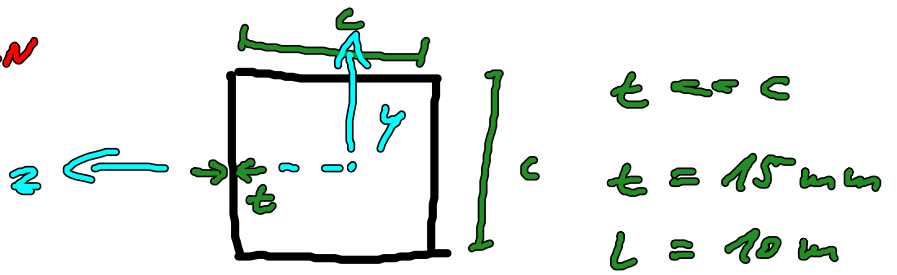
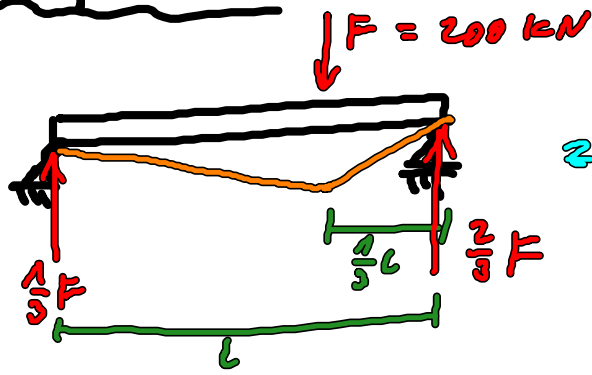
$$W = \frac{I_0}{|y_{max}|} = \frac{\frac{\pi}{4} (R_a^4 - R_i^4)}{R_a}$$

$$\Rightarrow \frac{F \cdot L \cdot 4 \cdot R_a}{\pi (R_a^4 - R_i^4)} \leq \sigma_{zul} \Rightarrow F \leq \frac{\sigma_{zul} \pi (R_a^4 - R_i^4)}{4L \cdot R_a}$$

mit Zahlenwerten:

$$F \leq 2,9 \cdot 10^3 \text{ N}$$

Beispiel 2:



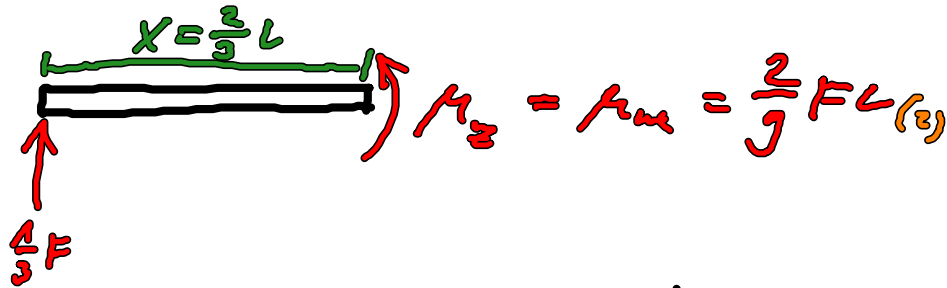
$$t \ll c$$

$$t = 15 \text{ mm}$$

$$L = 10 \text{ m}$$

ges: c damit $\sigma_{\text{max}} \leq \sigma_{\text{zul}} = 200 \text{ MPa}$

$$\sigma_{\text{zul}} = \frac{|M_{\text{max}}|}{W} \quad (1)$$



$$M_{\text{max}} = ?$$

$$W = \frac{I}{12 \text{ mm}} = \frac{I_a - I_i}{c} = \frac{2 \left(\frac{1}{12} c^3 - \frac{1}{12} (c-2t)^3 \right)}{c}$$

$$= \frac{(\cancel{c^3} - \cancel{c^3} + 8c^2t - 24\cancel{ct^2} + 32\cancel{t^3} - 16\cancel{t^3})}{6c} = \frac{4}{3} c^2 t \quad (2)$$

(2), (1) in (1):

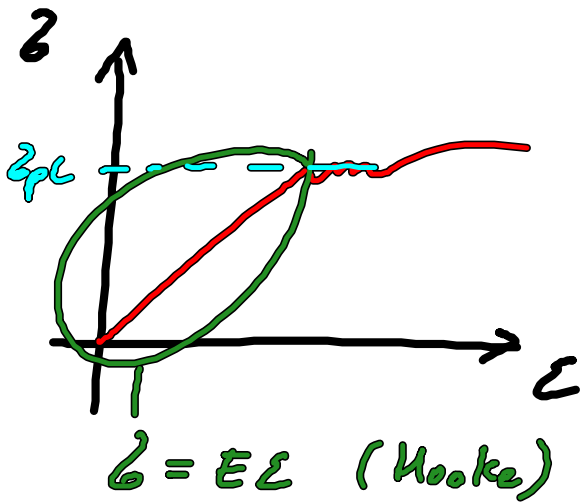
$$\frac{\frac{2}{9} FL}{\frac{4}{3} c^2 t} \leq \sigma_{\text{zul}} \Rightarrow c \geq \left(\frac{FL}{6t \sigma_{\text{zul}}} \right)^{\frac{1}{2}} = \underline{\underline{0,333 \text{ m}}}$$

II) Versagen beim Biegen:

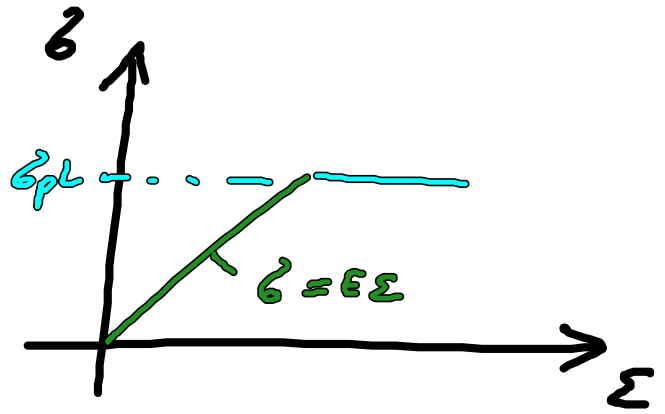


$$\epsilon = \frac{\Delta L}{L}$$

Spannungs-Dehnungsdiagramm

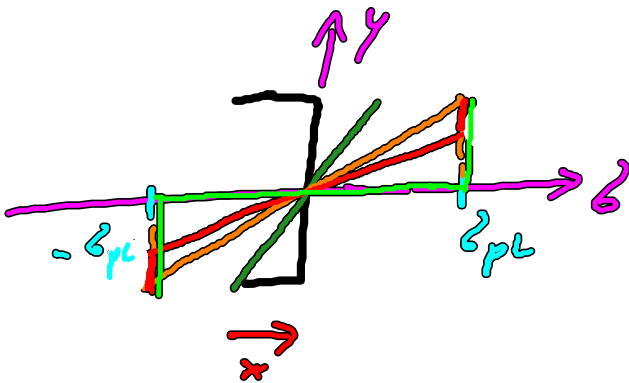
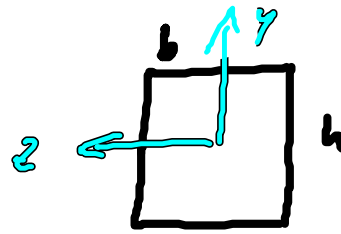
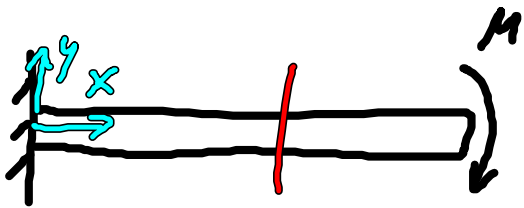


Näherung
→



ist σ_{pl} erreicht, erhöht sich σ nicht mehr mit ε

Beispiel:



$$\sigma_{max} = \frac{M}{W}$$

$$\sigma_{max} = \sigma_{pl}$$

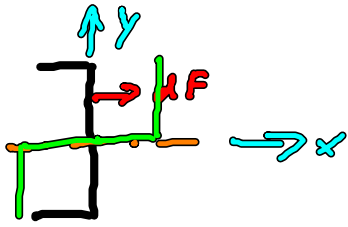
im Außenbereich ist $\sigma = \sigma_{pl}$

komplett plastisch verformt!

→ Wann tritt Versagen auf?



a) plastisches Versagen



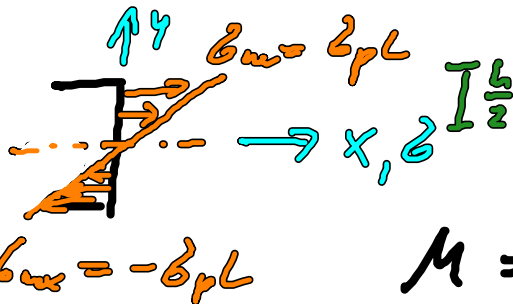
$$dM = -y dF = -y \sigma dA = -y \sigma b dy$$

$$M = \int_{-\frac{h}{2}}^{\frac{h}{2}} -y \sigma b dy = \int_0^{\frac{h}{2}} -y \sigma_{pl} b dy + \int_{-\frac{h}{2}}^0 -y (-\sigma_{pl}) b dy$$

$$M = \sigma_{pl} b \left(\left[-\frac{1}{2} y^2 \right]_0^{\frac{h}{2}} + \left[\frac{1}{2} y^2 \right]_{-\frac{h}{2}}^0 \right) = -b \sigma_{pl} \frac{h^2}{4}$$

$$\Rightarrow \boxed{M_{pl} = \frac{b h^2}{4} \sigma_{pl}} \Rightarrow \sigma = \sigma_{pl}$$

e) elastisches Versagen



$$\sigma = \frac{\sigma_{pl}}{\frac{h}{2}} y = \frac{2 \sigma_{pl}}{h} y$$

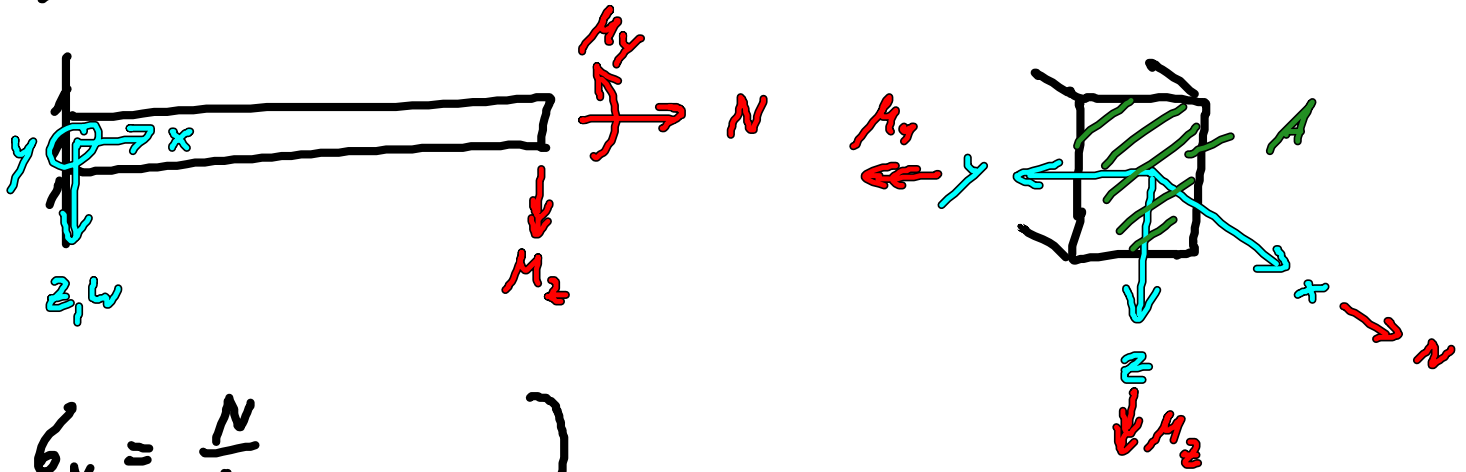
$$M = \int_{-\frac{h}{2}}^{\frac{h}{2}} -y b \sigma dy = \int_{-\frac{h}{2}}^{\frac{h}{2}} -\frac{2 \sigma_{pl}}{h} b y^2 dy$$

$$M = \left[-\frac{2}{3} \frac{\sigma_{pl}}{h} b y^3 \right]_{-\frac{h}{2}}^{\frac{h}{2}} = -\frac{1}{6} b \sigma_{pl} h^2$$

$$\Rightarrow \boxed{M_{el} = \frac{b h^2}{6} \sigma_{pl}} \Rightarrow \text{h. der Randfaser } \sigma = \sigma_{pl}$$

Vergleich: $\frac{M_{pl}}{M_{el}} = \frac{\frac{1}{4}}{\frac{1}{6}} = \frac{3}{2} = 1,5$

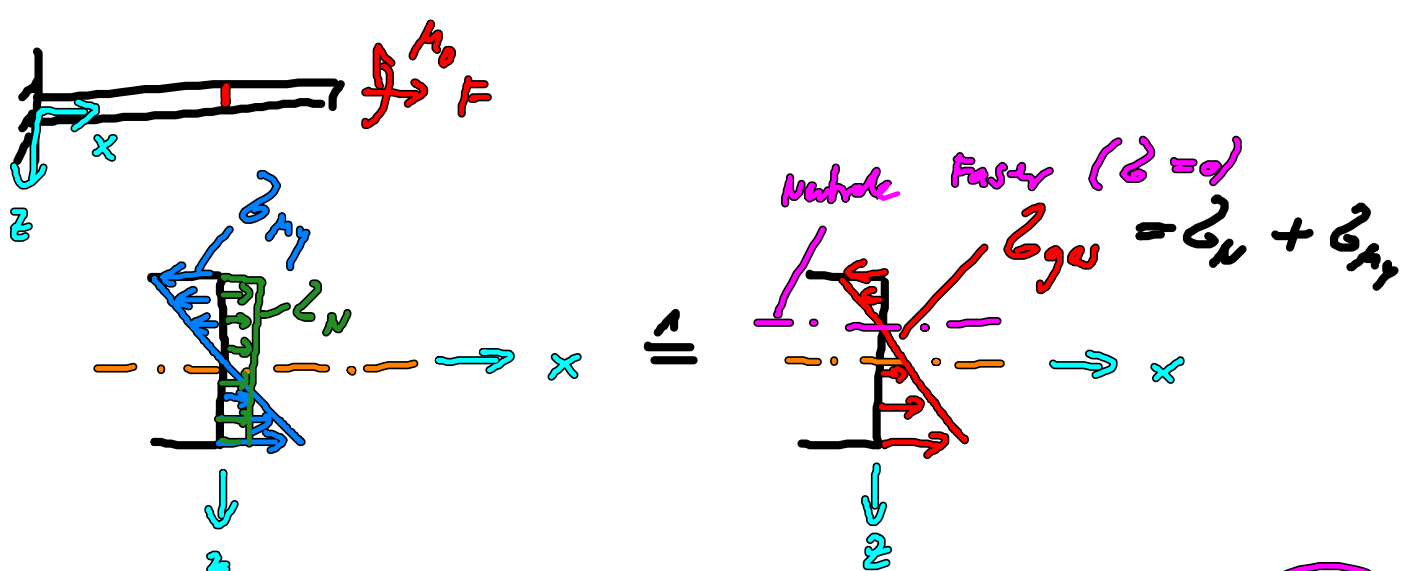
II) Überlagerung von Belastungen



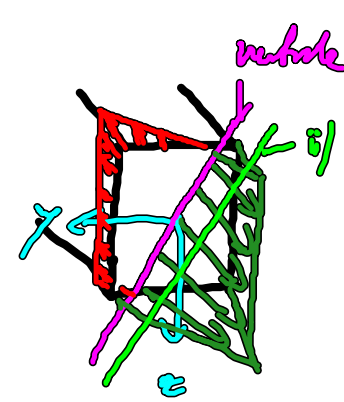
$$\left. \begin{aligned} \sigma_N &= \frac{N}{A} \\ \sigma_{M_2} &= -\frac{M_2}{I_z} \cdot y \\ \sigma_{M_y} &= \frac{M_y}{I_y} \cdot z \end{aligned} \right\}$$

$$\sigma = \sigma_N + \sigma_{M_2} + \sigma_{M_y}$$

$$\sigma = \frac{N}{A} - \frac{M_2}{I_z} \cdot y + \frac{M_y}{I_y} \cdot z$$

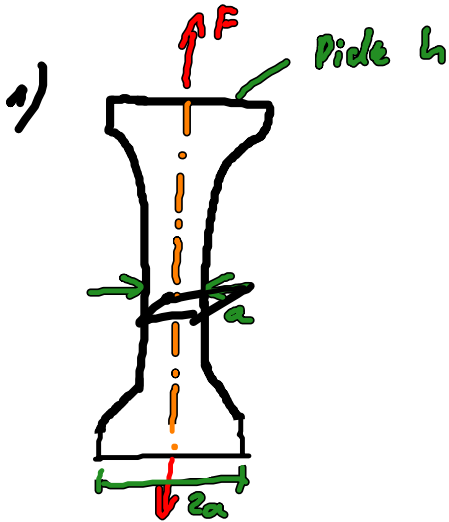


i) $N=0$: $0 = -\frac{M_2}{I_z} \cdot y + \frac{M_y}{I_y} \cdot z \Rightarrow z = \frac{M_z I_y}{I_z M_y} \cdot y$



ii) $N \neq 0 \Rightarrow z = \frac{M_2}{I_z} \frac{I_y}{M_y} \cdot y - N \frac{I_y}{M_y}$

Beispiel 3:



$$\sigma_1 = \frac{N}{A} = \frac{F}{A} = \frac{F}{2ah}$$

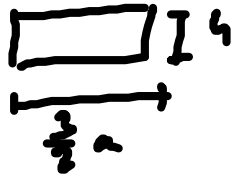
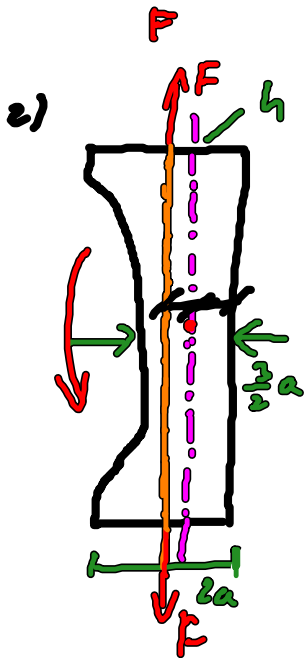


Kraft wirkt nicht in Sp

$$\sigma_2 = \frac{N}{A} + \frac{M_y}{I_y} \cdot z = \frac{F}{\frac{3}{2}ah} + \frac{F(a - \frac{3}{2}a)}{I_y} \cdot 2$$

$$= \frac{F}{\frac{3}{2}ah} + \frac{\frac{1}{2}Fa}{I_y} \cdot 2$$

$$\sigma_{un} = \frac{F}{\frac{3}{2}ah} + \frac{Fa}{4 \frac{1}{12} h (\frac{3}{2}a)^3} \cdot \frac{1}{4} a = \frac{4F}{3ah}$$



$$\sigma_{un}^1 = \frac{F}{ah}, \quad \sigma_{un}^2 = \frac{4F}{3ah} \Rightarrow \sigma_{un}^2 > \sigma_{un}^1$$